### Fabrication of a large-format blazed grating with radial grooves

Grayscale lithography & thermal reflow for 3D patterning

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### Penn State Nanofabrication Laboratory



#### Figure: RAITH EBPG 5200 & 5200+ 100 keV EBL tools at PSU

Chad Eichfeld, Michael Labella, Fabien Grisé, The McEntaffer Group, et al.

- PSU Dept. of Astronomy & Astrophysics and PSU Materials Research Institute:
  - Custom diffraction gratings for soft x-ray and UV spectroscopy
- Focus on electron-beam lithography (EBL) for grating fabrication:
  - curved or fanned grooves with periods down to  $\gtrsim 100\,\text{nm}$
  - sawtooth surface reliefs (blazed gratings)
  - curved substrates [AXRO talk by Fabien Grisé]
- Gratings designed for a converging beam of a Wolter telescope?

### **1** Utility of gratings with radial grooves for x-ray optics

### **2** TASTE testing (nanofabrication development)

### 8 Prototyping & pattern functionalization strategies

### 4 Full-sized radial grating for OGRE development

# Parallel grooves in a collimated beam

• For a plane wave illuminating grooves with  $\mathbf{k}$  as the dispersion direction, with  $K \equiv 2\pi/d$ :

$$\begin{cases} \mathbf{k}_n \cdot \mathbf{\hat{x}} &= \mathbf{k}_i \cdot \mathbf{\hat{x}} + nK \\ \mathbf{k}_n \cdot \mathbf{\hat{z}} &= \mathbf{k}_i \cdot \mathbf{\hat{z}} \end{cases} \text{ for } n = 0, \pm 1, \pm 2 \dots$$

Assigning spherical coordinates to k<sub>i</sub> and k<sub>n</sub> yields the grating equation

$$\begin{cases} \sin(\beta_n)\sin(\gamma'_n) + \sin(\alpha)\sin(\gamma) = \frac{n\lambda}{d} \\ \gamma'_n = \gamma \\ \sin(\alpha) + \sin(\beta_n) = \frac{n\lambda}{d\sin(\gamma)} \end{cases}$$

• But what happens in a converging beam?



# Parallel grooves in a converging beam

• Each incident ray has a different direction depending on (*x*, *z*) on the grating:

$$\mathbf{k}_{i}(x,z) = \frac{2\pi}{\lambda L(x,z)} \left[ (X_{f} - x) \mathbf{k} - Y_{f} \mathbf{y} - z \mathbf{z} \right]$$

with 
$$L(x,z) = \sqrt{(X_f - x)^2 + Y_f^2 + z^2}$$

- This leads to  $\alpha$  depending on grating position:

$$\sin(\alpha) = \frac{\sin(\alpha_{\text{nom}}) + x/R_f}{\sqrt{1 + 2(x/R_f)\sin(\alpha_{\text{nom}}) + (x/R_f)^2}}$$

which causes *aberrations in the dispersed spectrum* through  $\beta_n$  depending on  $\alpha$ 



## Radial grooves in a converging beam

• Cash (1983) proposed a grating design with radial grooves that converge at the focal plane:

$$d(x,z) = \theta_d \sqrt{x^2 + z^2}$$

• Diffraction occurs in the angular direction while specular reflection occurs radially:

$$\begin{cases} \mathbf{k}_n \cdot \mathbf{\hat{a}} &= \mathbf{k}_i \cdot \mathbf{\hat{a}} + nK \\ \mathbf{k}_n \cdot \mathbf{\hat{g}} &= \mathbf{k}_i \cdot \mathbf{\hat{g}} \end{cases} \text{ for } n = 0, \pm 1, \pm 2 \dots$$

• It can be shown that, for  $|x| \ll z$ ,

$$\sin(\alpha) \approx \sin(\alpha_{\text{nom}}) \left[ 1 - \frac{1}{2} \cos^2(\alpha_{\text{nom}}) \frac{x^2}{z^2} \right]$$



## Radial grooves in a converging beam

- The approximation |x| << z is equivalent to stating that the radial grooves do not converge too quickly
- The condition of grazing incidence allows further approximation such that the *X*-position of the *n*<sup>th</sup> diffracted order is

$$X_{n,f} \approx X_f + \frac{n\lambda}{\theta_d} \left[ 1 - \underbrace{\frac{1}{2} \frac{x^2}{z^2} + \frac{R_f^2}{2z^2} - \frac{X_f x}{z^2}}_{\text{small}} \right],$$

which provides utility as a dispersive element for spectroscopy



### Blazed, radial grooves



$$\lambda_b = \frac{d\sin(\gamma)}{n} \left[\sin(\alpha) + (2\delta - \alpha)\right]$$

Diffraction efficiency is maximized at the blaze wavelength,  $\lambda_b$ 

Radial grooves with blazed facets enable high spectral resolving power & spectral sensitivity simultaneously

J. A. McCoy, AXRO 2023



### Why not do KOH etching?



The precision of a non-parallel groove layout is limited by cubic structure of crystalline Si

J. A. McCoy, AXRO 2023

### What is the TASTE process?

Thermally **Activated S**elective Topography **Equilibration** 

coined by Schleunitz, et al. (2014)

- In short, TASTE describes how grayscale EBL can be combined with polymer thermal reflow to create 3D structures in resist
- But there are other variants of TASTE...



Figure: Fig. 3 from Schleunitz, et al. (2014)

### **Binary EBL and thermal reflow**



#### Figure: Traditional thermal reflow process

#### cf. Kirchner, et al. (2014)

- Electron exposure with dose *D* reduces molecular weight *M*<sub>w</sub> via chain scission
- Exposed resist is soluble in developer; clear to substrate
- Remaining resist has a glass-liquid transition temperature *T*<sub>g</sub>
  - 100 °C  $\leq T_g \lesssim$  130 °C for PMMA (depends on  $M_w$ )
- $T \gtrsim T_g + 50$  °C treatment causes molten resist to equilibrate into a convex topography

# Grayscale EBL (GEBL)



# **Figure:** Properties of GEBL-processed resist processed that enable TASTE

- Dose-modulated electron exposure imparts lateral gradient in *M*<sub>w</sub>
  - $\implies \begin{array}{ll} D_1 < D_2 < D_3 \text{ yields} \\ M_{w,1} > M_{w,2} > M_{w,3} \end{array}$
- *M<sub>w</sub>*-dependent etch rates yields stepped structure
  - $\implies M_{w,1} > M_{w,2} > M_{w,3} \text{ yields} \\ h_1 > h_2 > h_3 = 0 \\ \text{(timed wet development)}$
- Doses determined from 3DPEC algorithm in GENISYS BEAMER using a resist-contrast curve

### Selective thermal reflow



**Figure:** Properties of GEBL-processed resist processed that enable TASTE

- Developed GEBL structure exhibits lateral gradient in *T<sub>g</sub>* 
  - $\implies \begin{array}{ll} M_{w,0} > M_{w,1} > M_{w,2} \text{ yields} \\ T_{g,0} > T_{g,1} > T_{g,2} \end{array}$
  - $\implies \textbf{Enables selective thermal} \\ \textbf{reflow at } T_{g,0} > T > T_{g,1} \\ \end{cases}$



4) Patterned resist can be selectively reflowed at  $T_{g,0} > T > T_{g,1}$ 



### **GEBL test patterns**

#### **GEBL process development**

- Start with 950k PMMA A3 resist
- Spin coat to  $\sim$  130 nm on silicon wafer

### Test patterns (parallel gratings)

- pattern A: 6-level staircase where each step is 140 nm wide
  ⇒ d = 840 nm period
- pattern B: 4-level staircase where each step is 100 nm wide
  ⇒ d = 400 nm period
- *pattern C*: modified version of pattern B



**Figure:** AFMs of GEBL test patterns in 130 nm-thick PMMA

McCoy, et al. (2018)

#### d = 840 nm period, $\sim 10^{\circ}$ blaze angle



McCoy, et al. (2018)

### **Thermal reflow**

#### $d = 400 \,\mathrm{nm}$ period, $\sim 27^\circ$ blaze angle



McCoy, et al. (2018)

## Pattern functionalization strategies

#### Ideas

- 1. Dry etch pattern into substrate
- 2. Cross-link resist with UV exposure
- 3. Aluminize PMMA with sequential infiltration synthesis

### Plan

- Consider replication for final application
  - nanoimprint lithography (NIL)
  - substrate conformal imprint lithography (SCIL)
- Make single grating for prototype testing
  - Directly coat PMMA with thin metal layer for soft x-ray reflectivity
  - Test grazing-incidence diffraction efficiency at synchrotron facility



Figure: Surface-relief mold for grating prototype patterned in 130 nm-thick PMMA McCoy, et al. (2020)

## TASTE grating prototype

#### Grating prototype

- Start from pattern B with d = 400 nm
- Pattern 50 mm by 7.5 mm for synchrotron beam (~18 h exposure at 8 nA)



**Figure:** AFM of GEBL-processed resist (*top*), resist following thermal reflow at 116 °C for 30 min (*bottom*)



**Figure:** Surface-relief mold for grating prototype patterned in 130 nm-thick PMMA McCoy, et al. (2020)

### TASTE grating prototype

- Use electron-beam physical vapor deposition (EBPVD) for 15 nm of Au with 5 nm of Ti for adhesion
- Diminished, yet still significant, blaze response observed
  - Measured at Advanced Light Source (Lawrence-Berkeley Nat'l Lab, USA)





McCoy, et al. (2020)

### Scaling to very large areas

- System integration for OGRE development calls for:
  - Compatibility with JET-X optics 3500 mm focal length
  - Grating positioned  $z_{cen} = 3000 \text{ mm}$  from focal plane
  - Patterning over 70 mm by 63 mm area on 6" optic with  $\sim$  3  $\mu m$  flatness
- Baseline  $d(0, z_{cen}) = 315.15 \text{ nm}$ such that d ranges from 311.5 nm to 318.8 nm ( $\theta_d \sim 20$  milliarcsec)
- SHAPEDETECTION fracture mode in BEAMER handles tilted lines



**Figure:** AFM of GEBL pattern: 315 nm period (*top*), fractured GPF (*bottom*)

### Anticipation of the electron fogging effect

- Previous long writes (binary EBL) in some cases have been found to incur variation in critical dimension (CD) from over-exposure
- Attributed to the fogging effect

$$\begin{split} \mathsf{PSF}(r) \propto \frac{1}{\alpha^2} \mathrm{e}^{-r^2/\alpha^2} + \frac{\eta}{\beta^2} \mathrm{e}^{-r^2/\beta^2} \\ &+ \frac{\Theta}{\gamma^2} \mathrm{e}^{-r^2/\gamma^2} \end{split}$$

- forward scatter:  $\alpha \sim nm$
- backscatter/proximity:  $\beta \sim$  tens µm
- fogging:  $\gamma \sim$  tens mm? value of  $\Theta$ ?



Figure: Fig. 1 from Hudek, et al. (2007)

tool-dependent rather than substrate-dependent

### Impact of the fogging effect

- 25 mm by 25 mm area: patterns develop as expected with nominal doses
- Test pattern in center of background grating: patterns are over-dosed with nominal doses
- Test pattern in center of background grating: patterns are close to targeted from  $\sim$  86 % of nominal doses



### Conclusions

- Master grating prototype; to be replicated by substrate conformal imprint lithography (SCIL) for OGRE
- EBL exposure for full 70 mm by 63 mm grating completed in  $\sim$  90 h at 30 nA (> 600 GB of data)
- Coated via EBPVD with 15 nm of Au for reflectivity and 5 nm of Ti for adhesion post thermal reflow
- Tested for spectral resolving power at PANTER X-ray Test Facility [AXRO talk by Alex Higley]



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